

# Energy-Efficient Backscatter Aided Uplink NOMA Roadside Sensor Communications Under Channel Estimation Errors

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**Abstract**—This work presents non-orthogonal multiple access (NOMA) enabled energy-efficient alternating optimization framework for backscatter aided wireless powered uplink sensors communications for beyond 5G intelligent transportation system (ITS). Specifically, the transmit power of carrier emitter (CE) and reflection coefficients of backscatter aided roadside sensors are optimized with channel uncertainties for the maximization of the energy efficiency (EE) of the network. The formulated problem is tackled by the proposed two-stage alternating optimization algorithm named AOBWS (alternating optimization for backscatter aided wireless powered sensors). In the first stage, AOBWS employs an iterative algorithm to obtain optimal CE transmit power through simplified closed-form computed through Cardano's formulae. In the second stage, AOBWS uses a non-iterative algorithm that provides a closed-form expression for the computation of optimal reflection coefficient for roadside sensors under their quality of service (QoS) and a circuit power constraint. The global optimal exhaustive search (ES) algorithm is used as a benchmark. Simulation results demonstrate that the AOBWS algorithm can achieve near-optimal performance with very low complexity, which makes it suitable for practical implementations.

**Index Terms**—Sensors to infrastructure communications, wireless powered roadside sensors, backscatter communications, beyond 5G ITS, energy efficiency, power allocation, imperfect channel estimation.

## I. INTRODUCTION

**A**N EFFECTIVE traffic monitoring system is essential for ITS to surveil the prevailing conditions across the road. ITS demands a wide range of sensors on the road to manage transportation in an intelligent, seamless, safe, and

secure manner. These sensors could monitor traffic patterns, determine optimum traffic routing, identify traffic accidents, and perform environmental measurements [1]. In such a large-scale network, it is very essential to collect and transmit information with little power consumption. These sensors consist of sensing, computation, and communication components that consume power. Backscatter communication is an emerging technology that provides a single infrastructure for jointly sensing and transmitting data with microwatt levels of power consumption [2].

Backscatter communications provide batteryless connectivity through RF energy harvesting [3]. This technique is very different from the general energy harvesting techniques where devices harvest energy for the operation of active RF transmissions [4], [5]. On the contrary, backscatter communication is a low complexity and low power technique that does not require any active RF transmission component. It allows transmitters to transfer their information to the backscatter reader (BR) installed on receivers by reflecting and modulating the RF carrier signals of CE. Such backscattering at transmitters is done through mismatching the impedance at the input of the antenna which results in varying reflection coefficients [6]. Its transmission consumes very little energy as compared to the conventional radio and its operation without active RF component results in much simpler and uncomplicated circuits. The implementation of the backscatter technique for the wirelessly powered sensors has been limited because of its limited coverage. Backscatter communication based on bistatic architecture has been proposed to mitigate this limitation [3], [7], [8]. In bistatic backscatter communication, the CE is dislocated from BR, which results in a more flexible network configuration and reduces the near-far effect. Therefore, it is much more suitable for future ITS to use bistatic backscatter aided roadside sensors.

## A. Related Literature

Recently, backscatter communication has shown great potential for large-scale massive internet of things (IoT) networks [9]. To achieve low latency, high spectral, and energy efficiency, NOMA is the key technology to serve a large number of roadside sensors. The integration of NOMA with backscatter communication has proven great potential

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for collecting information from multiple sensors through the same sub-channel in a non-orthogonal manner [10], [11]. The information of multiple roadside sensors can be multiplexed on the same sub-channel by tuning the value of the reflection coefficient of each roadside sensor to a different value. After tuning their reflection coefficients, multiple roadside sensors in the same cluster can be separated through the power domain. Then, the BR can decode the information of each roadside sensor by employing the power difference of their signals. The authors in [10], used the combination of time-division multiplexing access (TDMA) with NOMA as hybrid access schemes for monostatic backscatter communication. They improved the network performance in terms of throughput and outage probability. In [12], authors investigated the ergodic rate and outage probability for backscatter NOMA system that integrates downlink NOMA communication with backscatter device. The performance of NOMA-enabled backscatter communication in terms of successful decoding of an average number of bits at the reader is analyzed in [13]. In [14], authors explored NOMA backscatter communication for UAV application by optimizing UAV altitude and trajectory. Author in [15], jointly optimize backscatter time and power reflection coefficients for throughput maximization of the NOMA bistatic communication network. EE of the symbiotic system that integrates downlink NOMA communication with backscatter device is maximized in [16].

So far following research contributions explored backscatter-aided vehicular communications. The overview of different use cases of NOMA-enabled backscatter aided 6G vehicular networks is presented in [17]. In [18], authors formulate the joint optimization of BS and RSU power allocation for efficient backscatter enabled vehicular communication with NOMA. They considered a downlink scenario for cooperative NOMA communication, in which multiple RSUs are assisting BS to multicast the information to the vehicles along with backscatter tag to vehicles communication. A novel learning-based optimization framework for backscatter aided heterogeneous vehicular networks is presented in [19]. The authors in [20], analyzed the integration of passive sensors and uplink backscatter communication for vehicular technology. They demonstrated the use of piezoelectric transducers for passive sensing along with uplink backscatter communication for pedestrians' safety and validated it through their experiments. The contribution in [21], proposed backscatter-aided secure vehicle-to-vehicle communication for managing parking situations in VANETs. The backscatter technology for vehicular positioning is investigated in [22].

### B. Motivations and Contributions

Roadside sensors collect large amounts of information and send it to central computing servers through roadside units (RSUs) or base stations (BSs) for analysis [23]. Besides, RSUs can also transfer sensed information to the vehicles that exist in their coverage area. For instance, sensors detect the pedestrians in the crosswalk and transmit messages to RSUs through backscatter communication to notify the presence of pedestrians. Then, RSUs disseminate

TABLE I  
THE LIST OF DIFFERENT ABBREVIATIONS AND THEIR DEFINITIONS

Acronym	Definition
AOBWS	Alternating optimization for backscatter aided wireless powered sensors.
BR	Backscatter reader.
BS	Base station.
CCFP	Concave-convex fractional programming.
CE	Carrier emitter.
CSI	Channel state information.
EE	Energy efficiency.
ES	Exhaustive search.
IoT	Internet of things.
ITS	Intelligent transportation system.
KKT	Karush–Kuhn–Tucker.
NOMA	Non-orthogonal multiple access.
OCETP	Optimal CE transmit power.
OFDMA	Orthogonal frequency-division multiple access.
QoS	Quality of service.
RF	Radio frequency.
RSU	Road side unit.
SIC	Successive interference cancellation.
TDMA	Time-division multiplexing access.
UAV	Unmanned aerial vehicles.
VANET	Vehicular ad-hoc network.

this information to surrounding vehicles in their coverage [20]. Hence, such an interconnected transport system results in better decision-making that leads to the improved safety of the environment [2]. As the roadside sensors need to collect and transmit different useful information to the RSUs in an energy-efficient manner. Therefore, backscatter communications can be employed by the roadside sensors to send their sensed information to the nearest RSU in the uplink scenario [17], [20]. Besides, obtaining CSI is crucial for the performance analysis of backscatter communications. In practice, it is very challenging for the passive transmitter to guarantee the accuracy of CSI all the time [24]. Furthermore, the realization of backscatter enabled uplink sensor communications will demand advanced energy-efficient resource allocation (RA) frameworks. Their RA is incredibly challenging due to the diverse quality-of-service (QoS) requirements and their strong underlying dynamics. In literature, we believe that there is no energy-efficient RA optimization framework for NOMA-enabled backscatter aided uplink roadside sensors communication with channel uncertainties. Therefore, in this article, we proposed a novel alternating optimization framework for EE maximization of wireless powered backscatter aided uplink sensors communications for future generation ITS under imperfect CSI. Our major contribution is summarized as follows,

- A novel energy-efficient alternating optimization framework for NOMA-enabled wireless powered uplink sensor communication under imperfect CSI is proposed for ITS. The EE maximization problem is formulated under various QoS requirements of bistatic backscatter communications for roadside sensors. The EE is maximized under channel uncertainties by optimizing transmit power of CE and the reflection coefficient of roadside sensors.

The formulated problem is solved in two stages, which yields the proposed AOBWS algorithm.

- The proposed two-stage AOBWS algorithm provides optimal EE performance in very low computational complexity, which makes it suitable for practical implementations. The detailed complexity analysis of the proposed algorithm and benchmark algorithms is presented in the complexity analysis subsection.
- The efficacy of the proposed AOBWS algorithm is analyzed through numerical simulations and is compared with the global optimal ES algorithm as a benchmark. From obtained results, it is observed that AOBWS can achieve desired EE performance with affordable computational complexity for practical implementations.

The rest of the paper is organized as follows: The system model is provided in Section II. In Section III, we discussed the problem formulation with its solution for the energy-efficient wireless powered uplink sensor communication under channel uncertainties for ITS while Section IV presents the numerical results to verify the efficacy of the proposed AOBWS algorithm. Finally, Section V provides concluding remarks on our analysis and discusses future work. The definition of different acronyms and symbols used in this paper are respectively defined in Table I and II.

## II. SYSTEM MODEL

This work considers NOMA-enabled backscatter communication for wireless-powered passive sensors in ITS. The system model consists of a CE, multiple backscatters aided roadside sensors, and BR installed on RSU as depicted in Figure 1. Roadside sensors are multiplexed in various clusters, where each cluster consists of  $K$  sensors. Practically, It is desirable to have two or three sensors per cluster for low decoding complexity and to guarantee timing constraints [25]. Roadside sensors harvest RF energy from the RF carrier signal emitted by CE [26] and backscatter their information to the BR. It works in two operational modes, namely the transmission mode ( $T_t$ ) and energy harvesting mode ( $T_h$ ). These two modes of roadside sensor constitute one slot such that  $T_t + T_h = 1$ ,<sup>1</sup> where  $T_t > 0$  and  $T_h > 0$ . In transmission mode, each cluster of roadside sensors backscatters the RF carrier signal of CE to transmit its sensed information to the BR. This backscattering is carried out with the help of an RF transistor. It reflects the incident carrier RF signal with altered phase and magnitude through mismatching the impedance at the input of the antenna which results in varying reflection coefficients. In the energy harvesting mode, the roadside sensor harvests energy from incident RF signal instead of reflecting it for transferring information. This harvested energy is then reserved in the battery and is utilized to power its circuitry. For a more detailed description of backscatter enabled sensors, please refer to [25].

The uplink transmission scenario is considered in which one cluster of two roadside sensors is handled by a single CE

and BR. Both roadside sensors and BR communicate through single antennas. The forward channel link between CE and  $k^{th}$  roadside sensor is denoted by  $H_{f,k}$ , while  $H_{b,k}$  is used to denote the backscatter link between  $k^{th}$  roadside sensor and BR, for  $k \in \{1, 2\}$ . The channel coefficients of the forward and backscatter link consist of the following components, respectively.

$$H_{f,k} = d_{f,k}^{-\alpha} \times h_{f,k}, \quad (1)$$

and

$$H_{b,k} = d_{b,k}^{-\alpha} \times h_{b,k}, \quad (2)$$

where  $h_{f,k}$  and  $h_{b,k}$  represent fast fading component of forward and backscatter link, respectively.  $d_{f,k}$  and  $d_{b,k}$  are the distance from CE to  $k^{th}$  roadside sensor and  $k^{th}$  roadside sensor to BR, respectively.  $\alpha$  is used as a path-loss exponent. Let  $P_{ce}$  be the power of the carrier signal emitted from CE. Then, the power of the incident RF signal at  $k^{th}$  roadside sensor is

$$P_k^I = P_{ce} |H_{f,k}|^2. \quad (3)$$

The roadside sensor can harvest energy from RF signals in both energy harvesting mode and transmission mode. Therefore, the energy harvested by  $k^{th}$  roadside sensor during transmission mode ( $T_t$ ) and energy harvesting mode ( $T_h$ ) is given as follows

$$P_k^{H_t} = \xi(1 - \Gamma_k)P_k^I T_{t,k}, \quad (4)$$

and

$$P_k^{H_h} = \xi P_k^I T_{h,k}, \quad (5)$$

where  $\xi$  denotes the efficiency of energy harvester while  $\Gamma_k$  represents reflection coefficient of  $k^{th}$  roadside sensor, where  $0 < \Gamma_k \leq 1$ . The reflected signal from  $k^{th}$  roadside sensor toward BR installed on RSU is

$$s_k = \sqrt{P_{ce}\Gamma_k} H_{b,k} x_k, \quad (6)$$

where  $x_k$  is the transmitted signal form  $k^{th}$  roadside sensor, satisfying  $\mathbb{E}(|x_k|^2) = 1$ . Then, the signal received at RSU is given as

$$y = \sum_{k=1}^2 H_{f,k} s_k + n, \quad (7)$$

or

$$y = \sum_{k=1}^2 \sqrt{P_{ce}\Gamma_k} H_{f,k} H_{b,k} x_k + n, \quad (8)$$

where  $H_k = H_{f,k} H_{b,k}$  is the overall channel link between  $k^{th}$  roadside sensor and BR, which can be estimated through LMMSE method [24].  $H_k$  can be written as  $H_k = d_k \times h_k$  [27], where  $d_k = d_{b,k}^{-\alpha} \times d_{f,k}^{-\alpha}$  and  $h_k = h_{b,k} \times h_{f,k}$ . In practice, it is very challenging for backscatter aided communications to guarantee accurate CSI at all the times [24]. Therefore, it is necessary to investigate the backscatter aided sensors to RSU communication with imperfect CSI. Under imperfect CSI estimation,  $H_k$  can be expressed by using the minimum

<sup>1</sup>Optimizing time coefficients of transmission mode  $T_t$  and energy harvesting mode  $T_h$  of the roadside sensor can further enhance the EE performance, however, it is left for our future work to focus here on optimizing CE transmit power and reflection coefficient of roadside sensors under channel uncertainties.

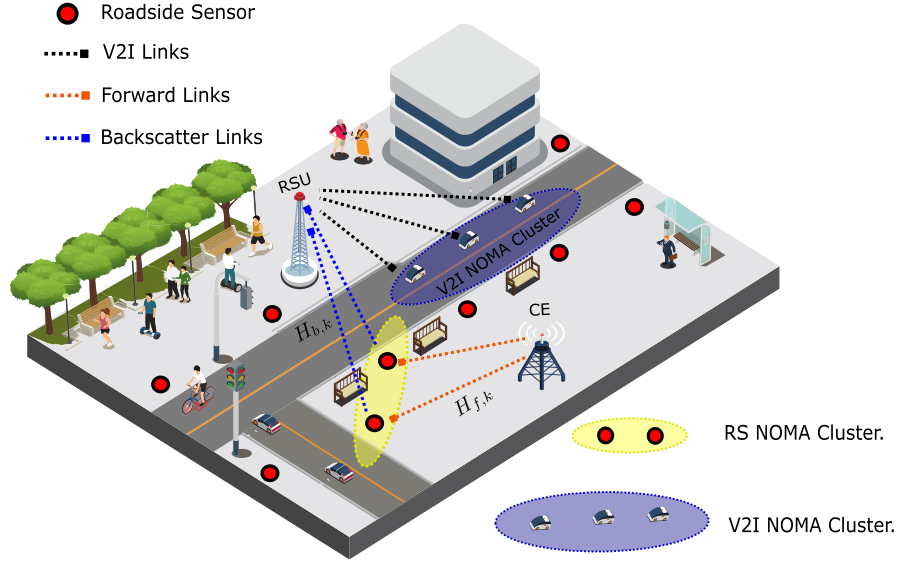


Fig. 1. Illustration of system model.

mean square error (MMSE) channel estimation error model [28], [29] as follow

$$H_k = \hat{H}_k + \epsilon_k, \quad (9)$$

where  $\hat{H}_k \sim \mathcal{CN}(0, \sigma_{\hat{H}_k}^2)$  is the estimated channel gain with variance  $\sigma_{\hat{H}_k}^2 = d_k - \sigma_{\epsilon_k}^2$  [30], while  $\epsilon_k \sim \mathcal{CN}(0, \sigma_{\epsilon_k}^2)$  is the estimated channel error, which is Gaussian distributed with zero mean and variance  $\sigma_{\epsilon_k}^2$ . The relative channel error can be represented as  $\rho_k = \frac{\sigma_{\epsilon_k}^2}{d_k}$ . Then,  $\sigma_{\epsilon_k}^2 = \rho_k d_k$  and  $\sigma_{\hat{H}_k}^2 = (1 - \rho_k) d_k$  [31]. For convenience of analysis, the case of constant estimation error ( $\sigma_{\epsilon_k}^2 = \sigma_{\epsilon}^2$ ) for all NOMA users is considered in this paper [30], [32]. Thus, the signal received at RSU under imperfect CSI is given as

$$\hat{y} = \sum_{k=1}^2 \sqrt{P_{ce}\Gamma_k} \hat{H}_k x_k + \epsilon \sum_{k=1}^2 \sqrt{P_{ce}\Gamma_k} x_k + n. \quad (10)$$

Without loss of generality, roadside sensors channel gains are arranged as:  $|\hat{H}_2|^2 > |\hat{H}_1|^2$ . Unlink downlink scenario, In the uplink, all information received at RSU from a cluster of roadside sensors are desired signals, although they give rise to multiuser interference. In downlink NOMA, SIC is implemented in ascending order i.e. the roadside sensor with lower channel gain is first decoded and removed. While in the uplink, the RSU can decode the roadside sensors signals in an arbitrary order, as all information is desired at the RSU [33]. However, despite that, to implement SIC and decode the received information at the RSU, tuning the value of the reflection coefficient of each roadside sensor to different values should be exploited in such a way that it maintained the distinctness among various signals. For the analysis, we assume that the SIC order that decodes the information of the 2nd roadside sensor (highest channel gain) first is employed at the RSU throughout this work [34]. According to the NOMA principles, the sum rate of roadside

sensors is given by

$$R = BW T_{t,1} \log_2(1 + \gamma_1) + BW T_{t,2} \log_2(1 + \gamma_2), \quad (11)$$

where

$$\gamma_1 = \left( \frac{P_{ce}\Gamma_1 |\hat{H}_1|^2}{\sigma_{\epsilon}^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2} \right), \quad (12)$$

and

$$\gamma_2 = \left( \frac{P_{ce}\Gamma_2 |\hat{H}_2|^2}{P_{ce}\Gamma_1 |\hat{H}_1|^2 + \sigma_{\epsilon}^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2} \right). \quad (13)$$

The total power consumed by the cluster is the circuit power consumption of the roadside sensors in backscatter mode. The circuit operation is performed through the harvested power from the carrier signal during transmission mode as well as in energy harvesting mode. The power consumed by the cluster can be obtained by the sum of the harvested powers of roadside sensors paired in that cluster. Besides it, total energy consumption also consists of the energy consumed by the CE to transmit RF signals and RSU to receive the signals of roadside sensors. Therefore, the total power consumption of the system is as follows

$$P_T = \sum_{k=1}^2 \frac{P_{ce}}{\kappa_k} (T_{t,k} + T_{h,k}) + P_{ce}^c + P_{RSU}^c, \quad (14)$$

where  $\kappa_k$  is power amplifier efficiency that ranges between zero and one while  $P_{ce}^c$  and  $P_{RSU}^c$  are the constant circuit power consumed by CE and RSU respectively. The energy efficiency of the proposed system model is defined as the ratio of the sum rate of the roadside sensor to the consumed power of the system in bits per Hertz per Joule (bits/Hz/J) [35], [36] as follows

$$EE = \frac{R}{P_T}. \quad (15)$$



TABLE II  
THE LIST OF DIFFERENT SYMBOLS AND THEIR DEFINITIONS

Symbol	Definition
$H_{f,k}$	Forward link channel coefficients of $k^{th}$ roadside sensor.
$H_{b,k}$	Backscatter link channel coefficients of $k^{th}$ roadside sensor.
$h_{f,k}$	Forward link fast fading component of $k^{th}$ roadside sensor.
$h_{b,k}$	Backscatter link fast fading component of $k^{th}$ roadside sensor.
$d_{f,k}$	Distance from CE to $k^{th}$ roadside sensor.
$d_{b,k}$	Distance from $k^{th}$ roadside sensor to BR.
$\alpha$	Path loss exponent.
$P_k^I$	Power of incident RF signal at $k^{th}$ roadside sensor.
$P_{ce}$	CE transmit power.
$P_k^{H_t}, P_k^{H_h}$	Energy harvested by $k^{th}$ roadside sensor during transmission mode and energy harvesting mode.
$\xi$	Efficiency of energy harvester.
$\Gamma_k$	Reflection coefficient of $K^{th}$ roadside sensor.
$s_k$	Reflected signal from $k^{th}$ roadside sensor towards BR.
$x_k$	Transmitted signal from $k^{th}$ roadside sensor towards BR.
$n, \sigma_n^2$	AWGN and its variance at RSU.
$H_k$	Overall channel link between $k^{th}$ roadside sensor and BR.
$\hat{H}_k, \epsilon_k$	Estimated channel gain and error of $k^{th}$ roadside sensor.
$\sigma_{\hat{H}_k}^2, \sigma_{\epsilon_k}^2$	Estimated channel and its error variance of $k^{th}$ roadside sensor.
$y$	Received signal at RSU with perfect CSI.
$\hat{y}$	Received signal at RSU with imperfect CSI.
$R, \bar{R}$	Sum-rate of roadside sensors before and after logarithmic approximation.
$\gamma_k$	SINR at $k^{th}$ roadside sensor.
$P_T$	Total power consumed by the cluster of sensors.
$P_{ce}^c, P_{RSU}^c$	CE and RSU circuit power.
$P_{RS}^c$	Roadside sensor circuit power.
$\lambda, \mu, \beta$	Lagrangian multipliers.
$\kappa_k$	Power amplifier efficiency.
$T_{t,k}, T_{h,k}$	Time coefficients of transmission and energy harvesting mode of $k^{th}$ roadside sensor.

### III. PROBLEM FORMULATION

Energy-efficient NOMA-enabled wireless powered passive sensors to infrastructure communication under imperfect CSI is the primary objective of the optimization problem. The energy efficiency maximization problem is formulated as

$$\begin{aligned} \max_{P_{ce}, \Gamma} EE &= \max_{P_{ce}, \Gamma} \frac{R}{P_T}, \\ \text{s.t. } C1 : P_{ce} \Gamma_1 |\hat{H}_1|^2 &\geq (2^{\frac{R_{min}}{T_{t,1}}} - 1) \left( \sigma_e^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2 \right), \\ C2 : P_{ce} \Gamma_2 |\hat{H}_2|^2 &\geq (2^{\frac{R_{min}}{T_{t,2}}} - 1) \left( P_{ce} \Gamma_1 |\hat{H}_1|^2 \right. \end{aligned}$$

$$\begin{aligned} &\left. + \sigma_e^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2 \right), \\ C3 : 0 &\leq P_{ce} \leq P_{max}, \\ C4 : 0 &< \Gamma_k \leq 1, k \in \{1, 2\}, \\ C5 : P_k^{H_h} + P_k^{H_t} &\geq P_{RS}^c T_{t,k}, k \in \{1, 2\}, \end{aligned} \quad (16)$$

where  $EE$  represents the energy efficiency of the wireless powered sensor communications in NOMA-enabled ITS.  $\Gamma = \{\Gamma_1, \Gamma_2\}$  is the vector of reflection coefficient of roadside sensors. C1 and C2 enforce roadside sensors to backscatter their information towards RSU with minimum QoS (minimum required rate) requirement. C3 ensures that the CE transmit power ( $P_{ce}$ ) cannot exceed its maximum transmit power ( $P_{max}$ ). C4 limits the reflection coefficient of sensors between 0 and 1. C5 guarantees that the energy harvested by the  $k^{th}$  sensor should exceed their minimum required circuit power ( $P_{RS}^c$ ).

The objective function defined in Eq. (16) has a non-linear fractional form, which is challenging to solve. The logarithmic approximation is implemented [37], which reduces complexity and transforms the optimization problem into tractable concave-convex fractional programming (CCFP) problem. The approximation is done as follows

$$\Pi \log_2(z) + \Phi \leq \log_2(1+z), \quad (17)$$

for any  $z \geq 0$ , where  $\Pi = \frac{z_0}{1+z_0}$  and  $\Phi = \log_2(1+z_0) - \frac{z_0}{1+z_0} \log_2(z_0)$ . When  $z = z_0$ , the bound becomes tight. Through lower bound of inequality in Eq. (17), the sum-rate of roadside sensors is presented as

$$\bar{R} = \sum_{k=1}^2 BW T_{t,k} (\Pi_k \log_2(\gamma_k) + \Phi_k), \quad (18)$$

where

$$\Pi_k = \frac{\gamma_k}{1+\gamma_k}, \quad (19)$$

and

$$\Phi_k = \log_2(1+\gamma_k) - \frac{\gamma_k}{1+\gamma_k} \log_2(\gamma_k). \quad (20)$$

Hence the updated optimization problem can be formulated as

$$\begin{aligned} \max_{P_{ce}, \Gamma} EE &= \max_{P_{ce}, \Gamma} \frac{\bar{R}}{P_T}, \\ \text{s.t. } C1 : P_{ce} \Gamma_1 |\hat{H}_1|^2 &\geq \left( 2^{\frac{R_{min}-T_{t,1}\Phi_1}{T_{t,1}\Pi_1}} \right) \left( \sigma_e^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2 \right), \\ C2 : P_{ce} \Gamma_2 |\hat{H}_2|^2 &\geq \left( 2^{\frac{R_{min}-T_{t,2}\Phi_2}{T_{t,2}\Pi_2}} \right) \left( P_{ce} \Gamma_1 |\hat{H}_1|^2 \right. \\ &\left. + \sigma_e^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2 \right), \\ C3 : 0 &\leq P_{ce} \leq P_{max}, \\ C4 : 0 &< \Gamma_k \leq 1, k \in \{1, 2\}, \\ C5 : P_k^{H_h} + P_k^{H_t} &\geq P_{RS}^c T_{t,k}. \end{aligned} \quad (21)$$

The EE maximization problem is coupled on two kinds of optimization variables i.e.,  $P_{ce}$ , and  $\Gamma$  in problem defined

in Eq. (21). Thus, it is very hard to find a globally optimal solution directly. It demands an approximate optimal algorithm through an alternating optimization algorithm. Therefore, this problem can be solved through an alternating optimization algorithm in two stages: *i*) In the first stage, on the fixed value of the reflection coefficient of roadside sensors, we compute the energy-efficient transmit power of the carrier emitter  $P_{ce}$ ; *ii*) we substitute the optimal  $P_{ce}^*$  obtained in stage 1 into the original problem and optimize the reflection coefficients of the roadside sensors in Stage 2.

#### A. Energy Efficient Transmit Power Allocation for CE

Given the reflection coefficients of roadside sensors, the optimization problem in Eq. (21) can be simplified to CE transmit power optimization as follow

$$\begin{aligned} \max_{P_{ce}} EE &= \max_{P_{ce}} \frac{\bar{R}}{P_T}, \\ \text{s.t. } &C1 - C3, C5. \end{aligned} \quad (22)$$

By using the following lemma, we demonstrate that  $\bar{R}$  is a concave function with respect to  $P_{ce}$ .

*Lemma 1:*

$$\begin{aligned} \bar{R} &= BWT_{t,1}(\Pi_1 \log_2 \left( \underbrace{\frac{P_{ce}\Gamma_1|\hat{H}_1|^2}{\sigma_e^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2}}_X \right) + \Phi_1) \\ &\quad + BWT_{t,2}(\Pi_2 \log_2 \left( \underbrace{\frac{P_{ce}\Gamma_2|\hat{H}_2|^2}{P_{ce}\Gamma_1|\hat{H}_1|^2 + \sigma_e^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2}}_Y \right) + \Phi_2) \end{aligned} \quad (23)$$

is a concave function with respect to  $P_{ce}$ .

*Proof:* Please, refer to Appendix A.

As,  $\bar{R}$  is concave with respect to  $P_{ce}$  and the objective function denominator is an affine function of  $P_{ce}$  in Eq. (22). Thus, the problem in Eq. (22) is in the form of a concave-convex fractional programming (CCFP) problem. Which can be solved efficiently through Dinkelbach's algorithm [38]. By using the Dinkelbach method, the problem in Eq. (22) can be transformed as

$$\begin{aligned} \max_{P_{ce}} EE &= \max_{P_{ce}} F(\psi) = \max_{P_{ce}} \bar{R} - \psi P_T, \\ \text{s.t. } &C1 - C3, C5, \end{aligned} \quad (24)$$

where  $\psi$  is the real parameter. Computing the roots of  $F(\psi)$  is analogous to solving the objective function in Eq. (22) [32].  $F(\psi)$  is negative when  $\psi$  approaches infinity, while  $F(\psi)$  is positive when  $\psi$  approaches minus infinity.  $F(\psi)$  is convex with respect to  $\psi$ . The convex problem in Eq. (24) is solved by employing the Lagrangian dual decomposition method. The Lagrangian function is presented in Eq. (25), shown at the bottom of the next page, where  $\mu = \{\mu_1, \mu_2\}$ ,  $\beta = \{\beta_1, \beta_2\}$ , and  $\lambda$  are the Lagrange multipliers. Constraints are KKT conditions for optimizing the power allocation for CE.

*Lemma 2:* The closed-form solution of optimal  $P_{ce}$  can be expressed as

$$P_{ce}^* = \sqrt[3]{q + \sqrt{q^2 + (r - p^2)^3}} + \sqrt[3]{q - \sqrt{q^2 + (r - p^2)^3}} + p \quad (26)$$

*Proof:* Please, refer to Appendix B

Given the optimal CE transmit power allocation policy in Eq. (26), the primal problem's Lagrangian multipliers can be determined and updated iteratively by employing the sub-gradient method as presented in Eqs. (27)–(31), shown at the bottom of the next page, where *iter* is used for iteration index.  $\omega_1, \omega_2, \omega_3, \omega_4$ , and  $\omega_5$  present positive step sizes. The appropriate step sizes should be used for the convergence to an optimal solution.

#### B. Efficient Selection of Reflection Coefficient for Roadside Sensor

Through simplified Cardano's formulae, a closed-form of optimal power for CE is obtained. Now the optimization problem for allocating efficient reflection coefficients to roadside sensors under their QoS and required circuit power constraint can be rewritten as,

$$\begin{aligned} \max_{\Gamma} \quad &\bar{R} - \psi P_T, \\ \text{s.t. } &C1 : P_{ce}^* \Gamma_1 |\hat{H}_1|^2 \geq \left( 2^{\frac{R_{min} - T_{t,1} \Phi_1}{T_{t,1} \Pi_1}} \right) \left( \sum_{k=1}^2 \sigma_e^2 P_{ce}^* \Gamma_k + \sigma_n^2 \right), \\ &C2 : P_{ce}^* \Gamma_2 |\hat{H}_2|^2 \geq \left( 2^{\frac{R_{min} - \Phi_2}{\Pi_2}} \right) \left( P_{ce}^* \Gamma_1 |\hat{H}_1|^2 \right. \\ &\quad \left. + \sum_{k=1}^2 \sigma_e^2 P_{ce}^* \Gamma_k + \sigma_n^2 \right), \\ &C3 : 0 < \Gamma_k \leq 1, k \in \{1, 2\}, \\ &C4 : \sum_{k=1}^2 \Gamma_k = \theta, \\ &C5 : P_k^{H_h} + P_k^{H_t} \geq P_{RS}^c T_{t,k}. \end{aligned} \quad (32)$$

To solve optimization problem defined in Eq. (32), first we will present in Lemma 3 that  $\bar{R}$  is a concave function with respect to  $\Gamma_1$  and  $\Gamma_2$ .

*Lemma 3:*

$$\begin{aligned} \bar{R} &= BWT_{t,1}(\Pi_1 \log_2 \left( \frac{P_{ce}^* \Gamma_1 |\hat{H}_1|^2}{\sigma_e^2 P_{ce}^* \theta + \sigma_n^2} \right) + \Phi_1) \\ &\quad + BWT_{t,2}(\Pi_2 \log_2 \left( \frac{P_{ce}^* \Gamma_2 |\hat{H}_2|^2}{P_{ce}^* \Gamma_1 |\hat{H}_1|^2 + \sigma_e^2 P_{ce}^* \theta + \sigma_n^2} \right) + \Phi_2) \end{aligned} \quad (33)$$

is a concave function with respect to  $\Gamma_1$  and  $\Gamma_2$ .

*Proof:* Please, refer to Appendix C

As,  $\bar{R}$  is concave with respect to  $\Gamma_1$  and  $\Gamma_2$ . Therefore maximum value of optimization problem defined in Eq. (32) can be obtained by the upper bound of reflection coefficient of roadside sensor as follow,

**Lemma 4:** The optimal reflection coefficient of the optimization problem defined in Eq. (32) is presented as

$$\Gamma_k^* = \max \left\{ \frac{2^{\aleph_k} (\sigma_T^2 + I_{NOMA})}{P_{ce}^* |\hat{H}_k|^2}, \min \left\{ 1 - \frac{P_{RS}^c}{P_k^I} + \frac{T_{h,k}}{T_{t,k}}, 1 \right\} \right\} \quad (34)$$

where,  $\aleph_k = \frac{R_{min} - T_{t,k} \Phi_1}{T_{t,k} \Pi_k}$ ,  $\sigma_T^2 = \sigma_e^2 P_{ce}^* \theta + \sigma_n^2$  and  $I_{NOMA} = \sum_{l=1}^{k-1} P_{ce}^* \Gamma_l |\hat{H}_l|^2$

*Proof:* For the given optimal  $P_{ce}^*$ , the objective function of optimization problem in Eq. (32) increases with increase of  $\Gamma$ . Therefore, the optimal reflection coefficient of the roadside sensor can be computed by the upper bound of the reflection coefficient. The range of  $\Gamma_k$  from the optimization problem in Eq. (32) can be determined by combining constraints C1, C3, and C5 for  $\Gamma_1$  and constraints C2, C3, and C5 for  $\Gamma_2$ . After some simple mathematical computations, the range of  $\Gamma_k$  can be presented as

$$\frac{2^{\aleph_k} (\sigma_T^2 + I_{NOMA})}{P_{ce}^* |\hat{H}_k|^2} \leq \Gamma_k \leq \min \left\{ 1 - \frac{P_{RS}^c}{P_k^I} + \frac{T_{h,k}}{T_{t,k}}, 1 \right\} \quad (35)$$

Thus, optimal  $\Gamma_k^*$  can be calculated as  $\max \left\{ \frac{2^{\aleph_k} (\sigma_T^2 + I_{NOMA})}{P_{ce}^* |\hat{H}_k|^2}, \min \left\{ 1 - \frac{P_{RS}^c}{P_k^I} + \frac{T_{h,k}}{T_{t,k}}, 1 \right\} \right\}$ .

Through Lemma 4, optimal reflection coefficients of roadside sensors can be determined. It is allocated to the roadside sensors in the following manner,

- When the condition  $\frac{2^{\aleph_k} (\sigma_T^2 + I_{NOMA})}{P_{ce}^* |\hat{H}_k|^2} \leq 1 - \frac{P_{RS}^c}{P_k^I} + \frac{T_{h,k}}{T_{t,k}} \leq 1$  is satisfied. Then, Lemma 4 will results in  $\Gamma_k^* = 1 - \frac{P_{RS}^c}{P_k^I} + \frac{T_{h,k}}{T_{t,k}}$ . This condition implies that the quality of service constraint and circuit power constraint of sensors is guaranteed simultaneously. In such condition,  $\Gamma_k^* = 1 - \frac{P_{RS}^c}{P_k^I} + \frac{T_{h,k}}{T_{t,k}}$  presents the portion of backscattering signal in received RF signal at roadside sensor during transmission mode  $T_t$  while remaining portion of received RF signal is used for harvesting.
- When the condition  $\frac{2^{\aleph_k} (\sigma_T^2 + I_{NOMA})}{P_{ce}^* |\hat{H}_k|^2} \leq 1 \leq 1 - \frac{P_{RS}^c}{P_k^I} + \frac{T_{h,k}}{T_{t,k}}$  is satisfied. Then, it implies that the energy harvested during energy harvesting mode  $T_h$  is enough for the circuit operation of the roadside sensor and in transmission mode  $T_t$  all the received RF signal at the roadside sensor can be used for backscattering for EE maximization. In this condition Lemma 4 results in  $\Gamma_k^* = 1$ . In this condition, if both sensors which are backscattering using NOMA result in a reflection coefficient of 1, then the reflection coefficient of the near sensor should be calculated as  $1 - \nu$ . The value of  $\nu$  can be selected in such a way to satisfy  $P_{ce}^* \Gamma_2 |\hat{H}_2|^2 - P_{ce}^* \Gamma_1 |\hat{H}_1|^2 \leq P_{gap}$  (SIC constraint) [34].
- When the condition  $\frac{2^{\aleph_k} (\sigma_T^2 + I_{NOMA})}{P_{ce}^* |\hat{H}_k|^2} > 1 - \frac{P_{RS}^c}{P_k^I} + \frac{T_{h,k}}{T_{t,k}}$  is satisfied. Then, it implies that QoS constraint and circuit power constraint of the roadside sensor can not be guaranteed simultaneously. In such case, optimization problem defined in Eq. (32) is infeasible.

$L(P_{ce}, \mu, \lambda, \beta)$

$$\begin{aligned} &= BW T_{t,1} \left( \Pi_1 \log_2 \left( \frac{P_{ce} \Gamma_1 |\hat{H}_1|^2}{\sigma_e^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2} \right) + \Phi_1 \right) + BW T_{t,2} \left( \Pi_2 \log_2 \left( \frac{P_{ce} \Gamma_2 |\hat{H}_2|^2}{P_{ce} \Gamma_1 |\hat{H}_1|^2 + \sigma_e^2 P_{ce} \sum_{k=1}^2 \Gamma_k + \sigma_n^2} \right) + \Phi_2 \right) \\ &\quad - \psi \left( \sum_{k=1}^2 \frac{P_{ce}}{\kappa_k} (T_{t,k} + T_{h,k}) + P_{ce}^c + P_{RSU}^c \right) + \mu_1 \left( P_{ce} \Gamma_1 |\hat{H}_1|^2 - \left( 2^{\frac{R_{min} - T_{t,1} \Phi_1}{T_{t,1} \Pi_1}} \right) \left( \sum_{k=1}^2 \sigma_e^2 P_{ce} \Gamma_k + \sigma_n^2 \right) \right) \\ &\quad + \mu_2 \left( P_{ce} \Gamma_2 |\hat{H}_2|^2 - \left( 2^{\frac{R_{min} - T_{t,2} \Phi_2}{T_{t,2} \Pi_2}} \right) \left( P_{ce} \Gamma_1 |\hat{H}_1|^2 + \sum_{k=1}^2 \sigma_e^2 P_{ce} \Gamma_k + \sigma_n^2 \right) \right) \\ &\quad + \lambda \left( P_{max} - P_{ce} \right) + \beta_1 \left( \xi (1 - \Gamma_1) P_{ce} |H_{f,1}|^2 T_{t,1} + \xi P_{ce} |H_{f,1}|^2 T_{h,1} - P_{RS}^c T_{t,1} \right) \\ &\quad + \beta_2 \left( \xi (1 - \Gamma_2) P_{ce} |H_{f,2}|^2 T_{t,2} + \xi P_{ce} |H_{f,2}|^2 T_{h,2} - P_{RS}^c T_{h,2} \right), \end{aligned} \quad (25)$$

$$\lambda(iter + 1) = \left[ \lambda(iter) - \omega_1(iter) (P_{max} - P_{ce}) \right]^+, \quad (27)$$

$$\mu_1(iter + 1) = \left[ \mu_1(iter) - \omega_2(iter) \left( P_{ce} \Gamma_1 |\hat{H}_1|^2 - \left( 2^{\frac{R_{min} - T_{t,1} \Phi_1}{T_{t,1} \Pi_1}} \right) \left( \sum_{k=1}^2 \sigma_e^2 P_{ce} \Gamma_k + \sigma_n^2 \right) \right) \right]^+, \quad (28)$$

$$\mu_2(iter + 1) = \left[ \mu_2(iter) - \omega_3(iter) \left( P_{ce} \Gamma_2 |\hat{H}_2|^2 - \left( 2^{\frac{R_{min} - T_{t,2} \Phi_2}{T_{t,2} \Pi_2}} \right) \left( P_{ce} \Gamma_1 |\hat{H}_1|^2 + \sum_{k=1}^2 \sigma_e^2 P_{ce} \Gamma_k + \sigma_n^2 \right) \right) \right]^+, \quad (29)$$

$$\beta_1(iter + 1) = \left[ \beta_1(iter) - \omega_4(iter) \left( \xi (1 - \Gamma_1) P_{ce} |H_{f,1}|^2 T_{t,1} + \xi P_{ce} |H_{f,1}|^2 T_{h,1} - P_{RS}^c T_{t,1} \right) \right]^+, \quad (30)$$

$$\beta_2(iter + 1) = \left[ \beta_2(iter) - \omega_5(iter) \left( \xi (1 - \Gamma_2) P_{ce} |H_{f,2}|^2 T_{t,2} + \xi P_{ce} |H_{f,2}|^2 T_{h,2} - P_{RS}^c T_{t,2} \right) \right]^+, \quad (31)$$

The details of the proposed algorithm AOBWS is summarized in Algorithm 1.

Once RSU received the information from roadside sensors, then that information can be provided to the vehicles through energy-efficient schemes proposed in [28] and [39].

**Algorithm 1** Alternating Optimization for Backscatter Aided Wireless Powered Sensors (AOBWS) Algorithm

- 1: **Stage 1: OCETP**
- 2: **Initialization:** Reflection coefficient of roadside sensor, maximum iterations  $I_{max}$ , and maximum tolerance  $\delta_{max}$ . Initialize the stepsizes and the dual variables( $\beta$ ,  $\mu$  and  $\lambda$ ) and iteration index  $I = 1$ .
- 3: **while**  $I \leq I_{max}$  **or**  $|\bar{R}(I) - \psi(I)P_T| \geq \delta_{max}$  **do**
- 4:   Compute  $\bar{R}(I)$  by using Eq. (18)
- 5:   Compute  $\psi(I) = \frac{\bar{R}(I)}{P_T}$
- 6:   Update dual variables  $\lambda(I)$  and  $\mu(I)$  and  $\beta(I)$  by using Eq. (27), (28), (29), (30), and (31), respectively.
- 7:   Update the transmit power  $P_{ce}(I+1)$  of CE by using equation (26) in **Lemma: 2**.
- 8:    $I = I + 1$ .
- 9: **end while**
- 10: **Output:** Optimal CE transmit power  $P_{ce}^*$ .
- 11: **Stage 2: Optimal Reflection Coefficient**
- 12: Under optimal  $P_{ce}^*$  obtained at stage 1, compute optimal reflection coefficient of roadside sensor through **Lemma: 4**.
- 13: **Output:** Optimal  $\Gamma^* = \{\Gamma_1^*, \Gamma_2^*\}$
- 14: **Algorithm 1 Output:** AOBWS = OCETP + Optimal reflection coefficient =  $P_{ce}^*$  and  $\Gamma^*$ .

### C. Complexity Analysis

This subsection presents the complexity analysis of the proposed AOBWS algorithm and ES algorithm as benchmark algorithm. In literature, ES algorithm is employed for NOMA optimal power allocation [40]. Moreover, it is also used as a benchmark algorithm [41], [42], [43], because it shows the best performance as compared to all other algorithms but at high computational complexity. In this article, ES algorithm is used as a benchmark because it obtains global optimal EE performance for the considered system model. It searches over all possible search points in the search regions of CE transmit power and reflection coefficients of the roadside sensor. However, it demands a large amount of computation as follows. If  $P_{max}$  is the maximum transmit power of CE and  $P_{step}$  is the step size for transmit power of CE. Then, there are  $(\frac{P_{max}}{P_{step}})$  choices for the values of transmit power of CE. Similarly, if  $\Gamma_{max}$  is the maximum value of reflection coefficient that can be assigned to the roadside sensor and  $\Gamma_{step}$  is the step size for reflection coefficient, then there are  $(\frac{\Gamma_{max}}{\Gamma_{step}})^K$  choices for the values of reflection coefficients of K sensors linked with BR installed on RSU. Therefore, the complexity of ES algorithm is  $\mathcal{O}(\frac{P_{max}}{P_{step}}) + \mathcal{O}(\frac{\Gamma_{max}}{\Gamma_{step}})^K$ . It can be noticed that the ES algorithm is computationally expensive but is used as a benchmark because of its global optimal solution.

TABLE III  
COMPLEXITY ANALYSIS OF ALGORITHMS

Algorithm	Complexity
Proposed AOBWS algorithm	$\mathcal{O}(IK^2 + K)$
ES algorithm (Benchmark)	$\mathcal{O}(\frac{P_{max}}{P_{step}}) + \mathcal{O}(\frac{\Gamma_{max}}{\Gamma_{step}})^K$

TABLE IV  
SIMULATION PARAMETERS

Parameter	Value
Bandwidth (BW)	1 MHz
CE Radius	5 m
Roadside sensors distribution around CE	BPP
Noise power ( $\sigma^2$ )	-114 dBm
Transmit power of CE ( $P_{ce}$ )	0 dBm - 40 dBm
Relative channel errors ( $\rho$ )	0.001 - 0.009
EH efficiency coefficient ( $\xi$ )	0.6
power amplifier efficiency ( $\eta$ )	(0, 1]
CE circuit power consumption ( $P_{ce}^c$ )	100 mW
RSU circuit power consumption ( $P_{RSU}^c$ )	1 W
Roadside sensor circuit power consumption ( $P_s^c$ )	-35 dBm
Roadside sensor minimum data rate $R_{min}$	0.5 bps/Hz
Path loss	distance dependent.
path-loss exponent ( $\alpha$ )	4
Fast fading	Rayleigh fading

For practical implementation AOBWS algorithm is proposed, which requires the complexity order of  $\mathcal{O}(IK^2 + K)$ .

AOBWS algorithm employs a two-stage procedure, in which the first stage consists of an iterative algorithm (OCETP) and 2nd stage is the non-iterative algorithm. OCETP algorithm during each iteration requires  $K$  operations to calculate EE. Where  $K$  is the total number of roadside sensors linked using NOMA with BR installed on RSU. Furthermore,  $K$  operations are required to update dual variables. If  $I$  is the number of iterations that the OCETP algorithm needs to converge, then the total complexity of the OCETP algorithm is  $\mathcal{O}(IK^2)$ . While in the 2nd Stage, AOBWS employs a non-iterative algorithm for optimal reflection coefficients, which requires  $K$  operations. After two-stage procedures, the complexity order of AOBWS becomes  $\mathcal{O}(IK^2 + K)$ . So, the proposed AOBWS algorithm is always less computationally complex as compared to the ES algorithm. When the number of  $K$  roadside sensors connected through NOMA with each RSU increases, the complexity of the ES algorithm increases exponentially while the proposed AOBWS algorithm still provides an optimal solution in polynomial time. The complexity analysis of the analyzed algorithms is presented in Table IV.

## IV. SIMULATIONS

This section presents the simulation results to evaluate the efficacy of the proposed algorithm in terms of energy efficiency and complexity. For this purpose, the proposed AOBWS algorithm is compared with the global optimal ES algorithm (benchmark algorithm). ES algorithm achieves global optimal solution but at the cost of high computational complexity and is impractical. It is observed the proposed AOBWS algorithm achieves very close performance to the global optimal ES with very low complexity and is therefore suitable for practical implementation. During simulations,



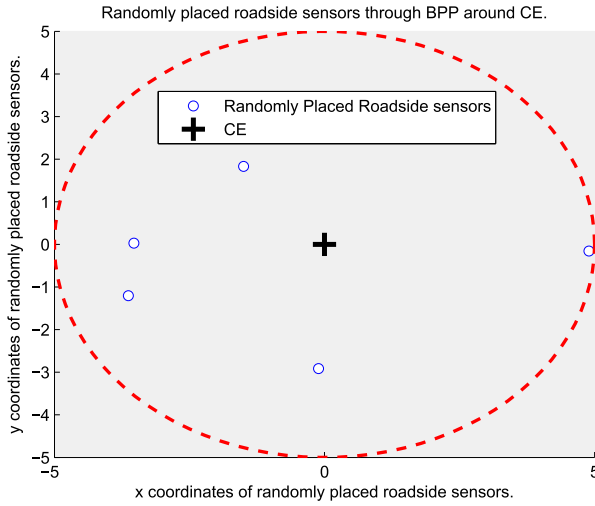


Fig. 2. Random distribution of roadside sensors around CE through BPP.

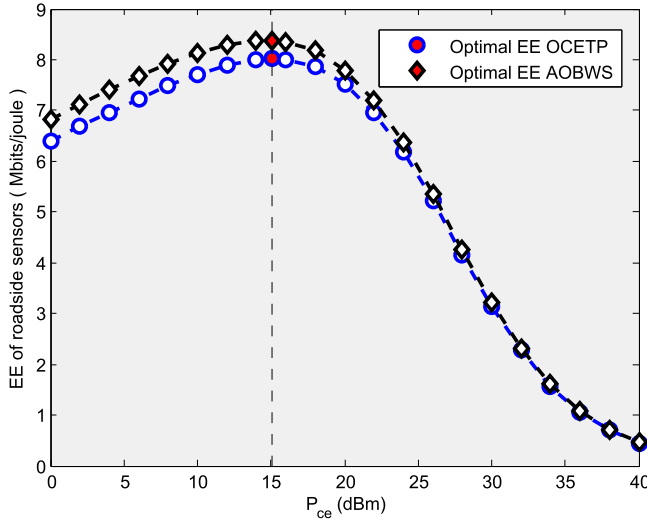


Fig. 3. Optimal EE of roadside sensors achieved through proposed OCETP and AOBWS.

roadside sensors are deployed randomly around the CE on the road and their locations are modelled as binomial point process (BPP) unless otherwise specified. In our simulations, each subchannel is serving two roadside sensors through NOMA, which are selected randomly from the generated sensors through BPP as shown in Fig. 2. The distance between the far roadside sensor to RSU and the near roadside sensor to RSU is set as 50 meters and 30 meters respectively unless otherwise specified. Time coefficient for roadside sensor transmission mode and energy harvesting mode is set to  $T_{t,1} = T_{t,2} = 0.5$  and  $T_{h,1} = T_{h,2} = 0.5$ . Other main simulation parameters for our considered system model are described in Table IV.

Fig. 3 presents the EE of roadside sensors versus the transmit power of CE in dBm. This figure provides the comparison of two proposed algorithms, where AOBWS refers to alternating optimization for backscatter aided wireless powered sensors, which provide optimal EE by optimizing both CE transmit power and reflection coefficient of the roadside sensor through the proposed alternating optimization framework. AOBWS optimizes CE transmit power under the given reflection coefficient of the roadside sensor in the first stage while in the 2nd stage it optimizes the reflection

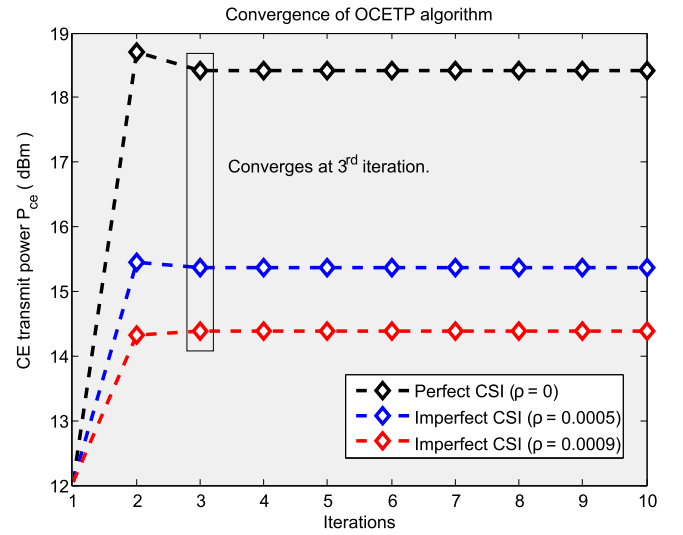


Fig. 4. Convergence of OCETP algorithm under various relative channel errors  $\rho$ .

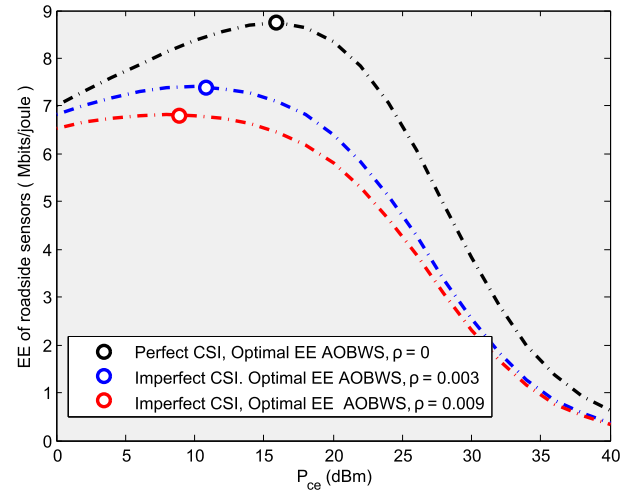


Fig. 5. Optimal EE through proposed AOBWS algorithm under various relative channel errors  $\rho$ .

coefficient of the roadside sensor under optimal CE transmit power obtained in the 1st stage. While OCETP refers to the first stage of AOBWS which obtains optimal CE transmit power under the given reflection coefficient of the roadside sensor. From the figure, it can be noticed that our proposed AOBWS has higher EE after performing its 2-stage operation as compared to OCETP.

As our proposed alternating optimization framework (AOBWS) consists of two stages, where the first stage employs an iterative algorithm for optimal CE transmit power named OCETP while in 2nd stage it uses a non-iterative algorithm for optimal reflection coefficient of roadside sensors. Therefore, it is vital to analyze the convergence of the OCETP algorithm. In Fig. 4, EE convergence of OCETP algorithm versus iterations is demonstrated with different relative channel errors ( $\rho$ ). The obtained result presents that the OCETP algorithm usually converges in three iterations regardless of  $\rho$ . It is observed that  $\rho$  affects EE, but their influence on the convergence of the OCETP algorithm is almost negligible.

Fig. 5 depicts optimal EE obtained by the proposed AOBWS algorithm under different relative channel errors. It can be

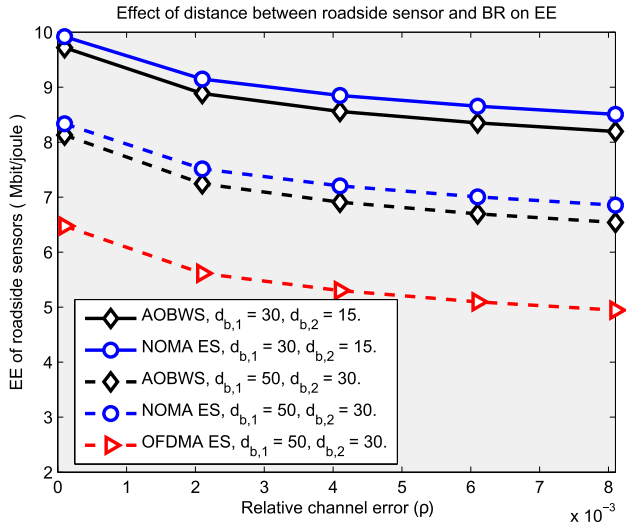


Fig. 6. EE of roadside sensors versus  $\rho$  under different distances between roadside sensor and BR.

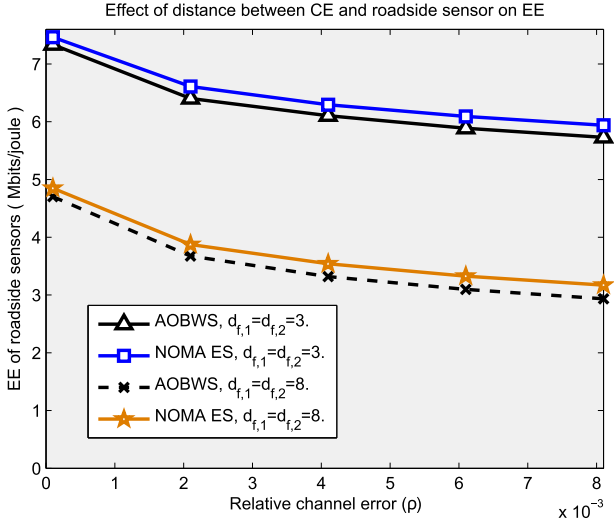


Fig. 7. EE of roadside sensors versus  $\rho$  under different distances between CE and roadside sensor.

observed from the figure that EE as a function of  $P_{ce}$  first increases and then decreases with increasing  $P_{ce}$ . It is because when  $P_{ce}$  is increased beyond the optimal  $P_{ce}^*$ , the roadside sensors sum-rate increases very slowly relative to the power consumption. It can also be examined from the figure that higher relative channel errors result in higher EE degradation.

Fig. 6 compares the EE of the proposed AOBWS algorithm with the global optimal ES algorithm and OFDMA. The comparison is done versus relative channel errors while considering different distances between roadside sensors and BR installed on RSU. It can be analyzed from the figure that AOBWS obtains very close EE performance to the ES algorithm with very low complexity. Moreover, it can be observed that higher relative channel error has a higher degrading effect on the EE. From the figure, it can also be noticed that a greater distance between roadside sensors and BR installed on RSU results in higher EE degradation.

In Fig. 7, the EE of the proposed AOBWS algorithm is compared with the global optimal ES algorithm versus relative channel errors. This figure presents the effect of distance between dedicated CE and roadside sensor. From the

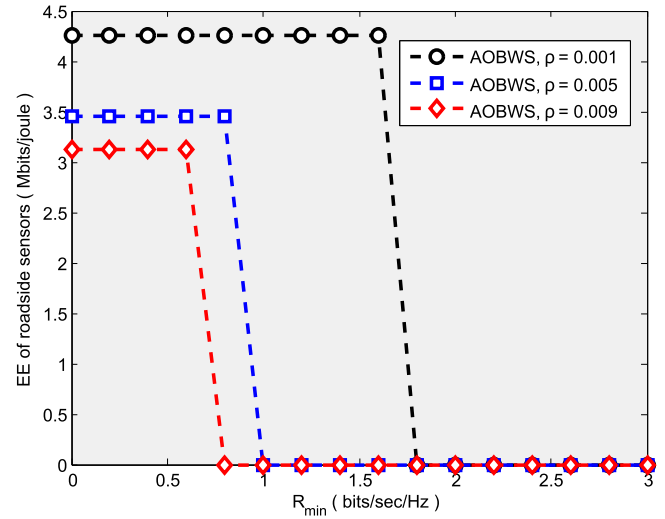


Fig. 8. EE of roadside sensors versus  $R_{min}$ .

results, It can be examined that a higher distance between CE and roadside sensor will result in lower EE. Moreover, the proposed AOBWS algorithm shows very close performance to the ES algorithm, which presents the efficacy of our proposed algorithm with low computational complexity.

Fig. 8 shows the EE of roadside sensor versus QoS requirement of the roadside sensor in terms of minimum data rate ( $R_{min}$ ) for the proposed AOBWS algorithm. The analysis of this figure is done with  $d_{f,1} = 10$ ,  $d_{f,2} = 5$ ,  $d_{b,1} = 50$ , and  $d_{b,2} = 30$ . This figure depicts that higher relative channel error will result in the lower guaranteed data rate of the network.

## V. CONCLUSION

In this article, we proposed an alternating optimization framework for backscatter aided wireless powered roadside sensors to infrastructure communications with imperfect CSI. By considering various QoS requirements of bistatic backscatter communications for roadside sensors, we aim to maximize the EE of the network. The EE is maximized under channel uncertainties by optimizing transmit power of CE and the reflection coefficient of roadside sensors, with very low computational complexity for practical implementations. The proposed problem for the solution is decoupled into two stages, which yields the proposed AOBWS algorithm. The complexity analysis of the proposed algorithm is analyzed in detail and compared with the global optimal ES algorithm. It is observed that our proposed algorithm can obtain near-optimal EE performance with very low complexity. Moreover, numerical results present the efficacy of our proposed result in terms of computational complexity and EE performance. In the future, we want to extend our work to a multi-cluster of roadside sensors, full-duplex (FD) roadside sensors, and multi-antenna roadside sensors.

## APPENDIX A

### CONCAVITY OF $\bar{R}$ WITH RESPECT TO $P_{ce}$

Appendix A presents the concavity of  $\bar{R}$  with respect to  $P_{ce}$ . The first derivative of  $\bar{R}$  w.r.t.  $P_{ce}$  is given as

$$\frac{\partial \bar{R}}{\partial P_{ce}} = \frac{BWT_{t,1}\Pi_1\sigma_n^2}{\ln(2)P_{ce}X} + \frac{BWT_{t,2}\Pi_2\sigma_n^2}{\ln(2)P_{ce}Y}. \quad (36)$$

The second order derivative is given as

$$\frac{\partial^2 \bar{R}}{\partial P_{ce}^2} = -\frac{V}{\ln(2)P_{ce}^2 X^2} - \frac{W}{\ln(2)P_{ce}^2 Y^2}. \quad (37)$$

where  $V = BW T_{t,1} \Pi_1 (\sigma_n^2) (2 \sum_{k=1}^2 \sigma_e^2 P_{ce} \Gamma_k + \sigma_n^2)$  and  $W = BW T_{t,2} \Pi_2 (\sigma_n^2) (2(P_{ce} \Gamma_1 |\hat{H}_1|^2 + \sum_{k=1}^2 \sigma_e^2 P_{ce} \Gamma_k) + \sigma_n^2)$ .

As second order derivative of  $\bar{R}$  i.e.  $\frac{\partial^2 \bar{R}}{\partial P_{ce}^2} < 0$ , therefore  $\bar{R}$  is concave and is an increasing function of  $P_{ce}$ .

#### APPENDIX B

##### DERIVATION OF CLOSED-FORM SOLUTION OF OPTIMAL $P_{ce}$

We exploit the KKT conditions such as

$$\frac{\partial L(P_{ce}, \mu, \lambda, \beta)}{\partial P_{ce}} \big|_{P_{ce}=P_{ce}^*} = 0. \quad (38)$$

The above equation results in

$$\frac{A}{\ln(2)P_{ce}(BP_{ce} + \sigma_n^2)} + \frac{C}{\ln(2)P_{ce}(DP_{ce} + \sigma_n^2)} + G = 0, \quad (39)$$

where

$$A = T_{t,1} BW \Pi_1 \sigma_n^2, \quad (40)$$

$$B = \sum_{k=1}^2 \sigma_e^2 \Gamma_k, \quad (41)$$

$$C = T_{t,2} BW \Pi_2 \sigma_n^2, \quad (42)$$

$$D = \Gamma_1 |\hat{H}_1|^2 + \sum_{k=1}^2 \sigma_e^2 \Gamma_k, \quad (43)$$

$$G = \sum_{k=1}^2 \mu_k Q_k + \sum_{k=1}^2 \beta_k P_k^H - \sum_{k=1}^2 \frac{\psi}{\kappa_k} - \lambda, \quad (44)$$

$$Q_k = \Gamma_k |\hat{H}_k|^2 - \left( 2^{\frac{R_{min} - T_{t,k} \Phi_k}{T_{t,k} \Pi_k}} \right) \left( \sum_{l=1}^{k-1} \Gamma_l |\hat{H}_l|^2 + \sum_{k=1}^2 \sigma_e^2 \Gamma_k \right), \quad (45)$$

and,

$$P_k^H = \xi(1 - \Gamma_k) |\hat{H}_{f,k}|^2 T_{t,k} + \xi \Gamma_k T_{h,k}. \quad (46)$$

After some computations

$$\begin{aligned} & (\ln(2)BDG)P_{ce}^3 + (\ln(2)BG\sigma_n^2 + \ln(2)DG\sigma_n^2)P_{ce}^2 \\ & + (\ln(2)G(\sigma_n^2)^2 + AD + CB)P_{ce} + (A\sigma_n^2 + C\sigma_n^2) = 0. \end{aligned} \quad (47)$$

The above equation can be solved through Cardano's formulae as follow

$$P_{ce}^* = \sqrt[3]{q + \sqrt{q^2 + (r - p^2)^3}} + \sqrt[3]{q - \sqrt{q^2 + (r - p^2)^3}} + p, \quad (48)$$

where,

$$p = \frac{-b}{3a}, \quad (49)$$

$$q = p^3 + \frac{bc - 3ad}{6a^2}, \quad (50)$$

$$r = \frac{c}{3a}, \quad (51)$$

and

$$a = \ln(2)BDG, \quad (52)$$

$$b = \ln(2)BG\sigma_n^2 + \ln(2)DG\sigma_n^2, \quad (53)$$

$$c = \ln(2)G(\sigma_n^2)^2 + AD + CB, \quad (54)$$

$$d = A\sigma_n^2 + C\sigma_n^2. \quad (55)$$

#### APPENDIX C

##### CONCAVITY OF $\bar{R}$ WITH RESPECT TO THE REFLECTION COEFFICIENTS OF ROADSIDE SENSORS

In the optimization problem defined in Eq. (32), we will present that  $\bar{R}$  is concave and is an increasing function of the reflection coefficient of roadside sensors. A function is concave if its Hessian matrix is negative definite. The Hessian matrix is negative definite if all eigenvalues are negative. Here we derive a Hessian matrix of  $\bar{R}$  and demonstrate it as a negative definite. The  $\bar{R}$  in optimization problem in Eq. (32) can be written as

$$\begin{aligned} \bar{R} &= T_{t,1} BW (\Pi_1 \log_2 \left( \frac{P_{ce} \Gamma_1 |\hat{H}_1|^2}{\sigma_e^2 P_{ce} \theta + \sigma_n^2} \right) + \Phi_1) \\ &+ T_{t,2} BW (\Pi_2 \log_2 \left( \frac{P_{ce} \Gamma_2 |\hat{H}_2|^2}{P_{ce} \Gamma_1 |\hat{H}_1|^2 + \sigma_e^2 P_{ce} \theta + \sigma_n^2} \right) + \Phi_2). \end{aligned} \quad (56)$$

The Hessian matrix of the above function with respect to  $\Gamma_1$  and  $\Gamma_2$  is defined as

$$H = \begin{bmatrix} \frac{\partial \bar{R}}{\partial \Gamma_1} & \frac{\partial \bar{R}}{\partial \Gamma_1 \partial \Gamma_2} \\ \frac{\partial \bar{R}}{\partial \Gamma_2} & \frac{\partial \bar{R}}{\partial \Gamma_2 \partial \Gamma_1} \end{bmatrix}, \quad (57)$$

where

$$\begin{aligned} \frac{\partial \bar{R}}{\partial \Gamma_1} &= \Upsilon_{1,1} \\ &= -\frac{T_{t,1} BW \Pi_1}{\ln(2) \Gamma_1^2} \\ &+ \frac{T_{t,2} BW \Pi_2 (P_{ce} |\hat{H}_1|^2)^2}{\ln(2) (P_{ce} \Gamma_1 |\hat{H}_1|^2 + (\sigma_e^2 P_{ce} \theta + \sigma_n^2)^2)}, \end{aligned} \quad (58)$$

$$\frac{\partial \bar{R}}{\partial \Gamma_1 \partial \Gamma_2} = \Upsilon_{1,2} = 0, \quad (59)$$

$$\frac{\partial \bar{R}}{\partial \Gamma_2 \partial \Gamma_1} = \Upsilon_{2,1} = 0, \quad (60)$$

and

$$\frac{\partial \bar{R}}{\partial \Gamma_2} = \Upsilon_{2,2} = -\frac{T_{t,2} BW \Pi_2}{\ln(2) \Gamma_2^2}. \quad (61)$$

Now the eigenvalues of the Hessian matrix can be calculated as follow

$$\begin{bmatrix} \Upsilon_{1,1} & \Upsilon_{1,2} \\ \Upsilon_{2,1} & \Upsilon_{2,2} \end{bmatrix} - \begin{bmatrix} \pi & 0 \\ 0 & \pi \end{bmatrix}. \quad (62)$$

$$\det \begin{pmatrix} \Upsilon_{1,1} - \pi & \Upsilon_{1,2} \\ \Upsilon_{2,1} & \Upsilon_{2,2} - \pi \end{pmatrix}, \quad (63)$$

det of above matrix results in,

$$\Upsilon_{1,1}\Upsilon_{2,2} - \pi\Upsilon_{1,1} - \pi\Upsilon_{2,2} + \pi^2 - \Upsilon_{1,2}\Upsilon_{2,1} = 0. \quad (64)$$

After writing it in standard form of  $Mx^2 + Nx + O$ ,

$$\pi^2 - (\Upsilon_{1,1} + \Upsilon_{2,2})\pi + (\Upsilon_{1,1}\Upsilon_{2,2} - \Upsilon_{1,2}\Upsilon_{2,1}) = 0, \quad (65)$$

where  $M = 1$ ,  $N = \Upsilon_{1,1} + \Upsilon_{2,2}$ ,  $O = \Upsilon_{1,1}\Upsilon_{2,2} - \Upsilon_{1,2}\Upsilon_{2,1}$

Then, the solution to the above problem is as follows

$$\pi = \frac{-N \pm \sqrt{N^2 - 4MO}}{2M}. \quad (66)$$

As the two possible eigenvalues computed through the above formulae are always negative for the hessian matrix, therefore  $\bar{R}$  is concave.

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